

Six-Phase Matrix Converter Fed Double Star Induction Motor

Bachir Ghalem, Bendiabdellah Azeddine

LDEE laboratory, University of Sciences and the Technology of Oran (USTO)
BP 1505 EL M'naouer Oran, Algeria, bachir@univ-usto.dz

Abstract: two different control strategies applied to a direct AC-AC six-phase matrix converter are investigated in the present paper. The first strategy is derived from the Venturini method, and the second approach is practically an extension of the scalar strategy control. Both strategies were originally applied to the three-phase matrix converter.

The current investigation deals with a comparative performance study of a double star induction motor fed from a six-phase matrix converter using the two above control strategies.

After a theoretical introduction of the six-phase matrix converter, a detailed description of the strategies implementation is presented followed by a discussion of results obtained from simulation results.

Keywords: six-phase; matrix converter; modulation coefficients; double star induction motor

1 Introduction

Over the last 20 years induction machines with a double star have been used in many industrial applications due to their performances in high power fields[4]. The double star induction machine requires a double three-phase supply and has many advantages. Not only does give reduced torque oscillations, but it also requires less powerful electronic components as the current flowing in a six-phase machine is less than that flowing in a three-phase machine. However, as the use of an inverter is necessary when feeding a double star induction machine, this may result in supplementary losses, since such an inverter is a harmonic generator[5].

A six-phase matrix converter can be used as a source for these kind machines, but the main problem is in finding the appropriate control method which produces a six-phase system with low electromagnetic torque oscillations.

2 Theory of the Matrix Converter

A matrix converter is a direct power converter, generating variable amplitude voltage and frequency from a rigid entry. An intermediate DC-link circuit is not necessary as in the classical inverter case. The principle of such a converter is based on a matrix topology connecting each input phase with each output phase by a two-way power switch, allowing the flow of power in both directions and therefore operating in all four quadrants. By using some well suited laws, the matrix converter can reproduce all the existing electronic power conversions (AC / AC, AC / DC, DC / DC and DC / AC).

The basic diagram of a matrix converter can be represented by Figure 1.

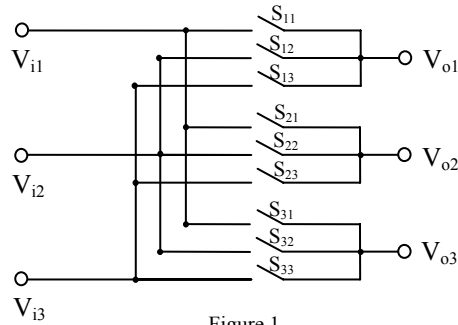


Figure 1

Basic circuit of a matrix converter

The symbol S_{ij} represents the ideal bidirectional switches, where i represents the index of the output voltage and j represents the index of the input voltage.

Let $[V_i]$ be the vector of the input voltages given as:

$$[V_i] = V_{im} \begin{bmatrix} \cos(\omega_i t) \\ \cos(\omega_i t - 2\pi/3) \\ \cos(\omega_i t - 4\pi/3) \end{bmatrix} \quad (1)$$

and $[V_o]$ the vector of desired output voltages.

$$[V_o] = V_{om} \begin{bmatrix} \cos(\omega_o t) \\ \cos(\omega_o t - 2\pi/3) \\ \cos(\omega_o t - 4\pi/3) \end{bmatrix} \quad (2)$$

The problem now consists in finding a matrix $[M]$ known as the modulation matrix, such that

$$[V_o] = [M] \cdot [V_i] \quad (3)$$

The development of the equation (3) gives:

$$\begin{bmatrix} V_{o1} \\ V_{o2} \\ V_{o3} \end{bmatrix} = \begin{bmatrix} m_{11} & m_{12} & m_{13} \\ m_{21} & m_{22} & m_{23} \\ m_{31} & m_{32} & m_{33} \end{bmatrix} \begin{bmatrix} V_{i1} \\ V_{i2} \\ V_{i3} \end{bmatrix} \quad (4)$$

where m_{ij} are the modulation coefficients.

During commutation, the bidirectional switches must function according to the following rules:

- At every instant t , only one switch S_{ij} ($i = 1,2,3$) works in order to avoid short-circuit between the phase.
- At every instant t , at least two switches S_{ij} ($j = 1,2,3$) works to ensure a closed loop load current.
- The switching frequency $f_s = \omega_s / 2\pi$ must have a value twenty times higher than the maximum of f_i, f_o ($f_s \gg 20 \cdot \max(f_i, f_o)$).
- During the period T_s known as the sequential period, which is equal to $1/f_s$. The sum of the time of conduction being used to synthesize the same output phase must be equal to T_s .

Now a time t_{ij} , called the modulation time, can be defined as:

$$t_{ij} = m_{ij} \cdot T_s \quad (5)$$

3 Theory of a Six-Phase Matrix Converter

The basic scheme of a six-phase matrix converter can be illustrated by Figure 2.

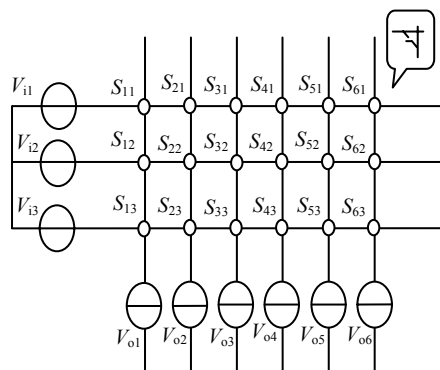


Figure 2

Basic scheme of a six-phase matrix converter

3.1 First Method

This method is derived from that proposed by Venturini [1], [2], [4] and has been used to solve the equation (3), from which a six-phase voltage system at the matrix converter output can be similarly obtained and represented by equation (6).

$$\begin{bmatrix} V_{o1} \\ V_{o2} \\ V_{o3} \\ V_{o4} \\ V_{o5} \\ V_{o6} \end{bmatrix} = \begin{bmatrix} m_{11} & m_{12} & m_{13} \\ m_{21} & m_{22} & m_{23} \\ m_{31} & m_{32} & m_{33} \\ m_{41} & m_{42} & m_{44} \\ m_{51} & m_{52} & m_{53} \\ m_{61} & m_{62} & m_{63} \end{bmatrix} \begin{bmatrix} V_{i1} \\ V_{i2} \\ V_{i3} \end{bmatrix} \quad (6)$$

The calculation of the m_{ij} coefficients in equation (6), will be the same as that for the m_{ij} coefficients for the case of a three phase[1], but expressed as follows:

$$[M] = \begin{bmatrix} m(3,3) & m(4,4) & m(5,5) \\ m(2,4) & m(3,5) & m(4,0) \\ m(1,5) & m(2,0) & m(3,1) \\ m(0,0) & m(1,1) & m(2,2) \\ m(5,1) & m(0,2) & m(1,3) \\ m(4,2) & m(5,3) & m(0,4) \end{bmatrix} \quad (7)$$

where the matrix coefficients are given in a general form as:

$$m(x_1, x_2) = \frac{1}{3} \alpha_1 [1 + 2QZ_1^{-1}(x_1)] + \alpha_2 [1 + 2QZ_1^{-1}(x_2)] \quad (8)$$

$$\text{where } Q = \frac{V_{om}}{V_{im}} \text{ and } Z_\alpha^\beta(y)(t) = \cos[(\alpha\omega_i + \beta\omega_o)t + y\frac{\pi}{3}]$$

$$\text{and } \alpha_1 = \frac{1}{2} \left(1 + \frac{\tan(\theta_i)}{\tan(\theta_o)} \right), \quad \alpha_2 = 1 - \alpha_1$$

with θ_i the phase of input voltages and θ_o the phase of output voltages.

As an example, the average value of the sixth output phase voltage during the k^{th} sequence can be expressed as:

$$V_{o6} = \begin{cases} V_{i1} & 0 \leq t - (k-1)T_s \leq m_{61}^k T_s \\ V_{i2} & m_{61}^k T_s \leq t - (k-1)T_s \leq (m_{61}^k + m_{62}^k) T_s \\ V_{i3} & (m_{61}^k + m_{62}^k) T_s \leq t - (k-1)T_s \leq (m_{61}^k + m_{62}^k + m_{63}^k) T_s \end{cases} \quad (9)$$

3.2 Second Method

The second method is derived from the scalar strategy control [3], [4]. A straightforward approach to generate the active and zero states of matrix switches in fig.1 consists of using the instantaneous voltage ratio of specific input phase voltages. Let us define the following phase voltages present at the input port as:

$$\begin{cases} V_A(t) = V_{im} \cos(\omega_i t) \\ V_B(t) = V_{im} \cos(\omega_i t - 2\frac{\pi}{3}) \\ V_C(t) = V_{im} \cos(\omega_i t - 4\frac{\pi}{3}) \end{cases} \quad (10)$$

At the output port of the converter, the value of any instantaneous output phase voltage may be expressed by equation (11) as follows:

$$V_o(t) = \frac{1}{T_S} (t_K V_K + t_L V_L + t_M V_M) \quad (11)$$

where $t_K + t_L + t_M = T_S$

K-L-M are variable subscripts, which may be assigned the variable A, B or C according to the following rules:

Rule 1: At any instant, the input phase voltage which has a polarity different from both others is assigned to “M”.

Rule 2: The two input phase voltages which share the same polarity, are assigned to K and L, the smallest one of the two, (in absolute value), being “K”. Then t_K and t_L are chosen such that:

$$\frac{t_K}{t_L} = \frac{V_K}{V_L} = \rho_{KL} \quad (12)$$

for the interval where

$$0 \leq \frac{V_K}{V_L} \leq 1 \quad (13)$$

The expressions given by equation (11) and equation (13) are similar to that ones originally proposed by [1]. Equation (12) defines the active time ratio between two out of the three switches, in one commutating leg of the output port (see Fig. 1). This time ratio (t_K/t_L) is proportional to the instantaneous voltage ratio (V_K/V_L) of their associated input phases. The ratio must be established with the smaller instantaneous voltage divided by the larger one, as stated in equation (13).

The converter switching pattern depends only on the scalar comparison of input phase voltages and the instantaneous value (V_o) of the desired output voltage. In

the following, the proper procedure to obtain the respective values of t_K , t_L and t_M during one period T_s of the sequence (or the carrier) frequency f_s is illustrated. For a specific interval where $0 \leq t_K/t_L \leq 1$.

The active times of the three switches associated with the desired output voltage V_o become:

$$t_K = \frac{T_s(V_o - V_M)}{(\rho_{KL}V_K + V_L - (1 + \rho_{KL})V_M)} \quad (14)$$

$$t_M = T_s(1 + \rho_{KL})V_L \quad (15)$$

Using again the current value of ρ_{KL} , equation (14) can be further developed such as:

$$t_L = \frac{T_s(V_o - V_K)V_L}{(V_K^2 + V_L^2 + V_M^2) + (V_K + V_L + V_M)V_M} \quad (16)$$

In a balanced three phase system, the summation of the three instantaneous phase voltage is zero. So the following relationships can be obtained:

$$\frac{t_L}{T_s} = \frac{T_s(V_o - V_K)V_L}{(V_K^2 + V_L^2 + V_M^2)} = \frac{T_s(V_o - V_K)V_L}{1.5V_{im}^2} \quad (17)$$

$$\frac{t_K}{T_s} = \frac{T_s(V_o - V_K)V_K}{1.5V_{im}^2} \quad (18)$$

$$\frac{t_M}{T_s} = 1 - \frac{(t_K - t_L)}{1.5V_{im}^2} \quad (19)$$

The duty cycle of commutators K and L is proportional to the instantaneous value of the corresponding input phase voltage V_K and V_L multiplied by the voltage difference between the desired output voltage V_o and the input phase voltage V_M . It should be noted at this point that the output voltage V_o , (i.e V_A , V_B , V_C), can be any kind of waveform, including DC values.

Solving equations (17, 18 and 19) for a given voltage ratio, $V_{om}/V_{im} = Q \leq 0.5$, will yield a positive value for the times t_K , t_L and t_M as in the case of the Venturini control algorithm.

The desired output voltages with which the coefficients are calculated are:

$$\left\{ \begin{array}{l} V_{o1} = V_{om} \cos(\omega_o t) \\ V_{o2} = V_{om} \cos(\omega_o t - \frac{\pi}{3}) \\ V_{o3} = V_{om} \cos(\omega_o t - 2\frac{\pi}{3}) \\ V_{o4} = V_{om} \cos(\omega_o t - 3\frac{\pi}{3}) \\ V_{o5} = V_{om} \cos(\omega_o t - 4\frac{\pi}{3}) \\ V_{o6} = V_{om} \cos(\omega_o t - 5\frac{\pi}{3}) \end{array} \right. \quad (20)$$

The development of equation (3) for the case of a six-phase matrix converter gives:

$$\begin{bmatrix} V_{o1} \\ V_{o2} \\ V_{o3} \\ V_{o4} \\ V_{o5} \\ V_{o6} \end{bmatrix} = \begin{bmatrix} m_{1K} & m_{1L} & m_{1M} \\ m_{2K} & m_{2L} & m_{2M} \\ m_{3K} & m_{3L} & m_{3M} \\ m_{4K} & m_{4L} & m_{4M} \\ m_{5K} & m_{5L} & m_{5M} \\ m_{6K} & m_{6L} & m_{6M} \end{bmatrix} \begin{bmatrix} V_K \\ V_L \\ V_M \end{bmatrix} \quad (21)$$

The average value of the voltage of the sixth output phase voltage during the K^{th} sequence is given as:

$$V_{o6} = \begin{cases} V_K & 0 \leq t - (k-1)T_s \leq m_{6K}^k T_s \\ V_L & m_{6K}^k T_s \leq t - (k-1)T_s \leq (m_{6K}^k + m_{6L}^k) T_s \\ V_M & (m_{6K}^k + m_{6L}^k) T_s \leq t - (k-1)T_s \leq (m_{6K}^k + m_{6L}^k + m_{6M}^k) T_s \end{cases} \quad (22)$$

4 Double Star Induction Machine Modelling

The mathematical model of the machine is written as a set of state equations, both for the electrical and mechanical parts [6], [8], [9]:

$$[V_{abc,s_1}] = [R_{s_1}][I_{abc,s_1}] + \frac{d[\Phi_{abc,s_1}]}{dt} \quad (23)$$

$$[V_{abc,s_2}] = [R_{s_2}][I_{abc,s_2}] + \frac{d[\Phi_{abc,s_2}]}{dt} \quad (24)$$

$$[V_{abc,r}] = [R_r][I_{abc,r}] + \frac{d[\Phi_{abc,r}]}{dt} \quad (25)$$

$$J \frac{d\Omega}{dt} = T_{em} - T_r - k_f \Omega \quad (26)$$

where J is the moment of inertia of the revolving parts, K_f is the coefficient of viscous friction, arising from the bearings and the air flowing over the motor, and T_{em} is the load torque.

The electrical state variables in the “ dq ” system are the flux represented by vector $[\Phi]$, while the input variable in the “ dq ” system are expressed by vector $[V]$.

$$\frac{d\Phi}{dt} = [A][\Phi] + [B][V] \quad (27)$$

$$[\Phi] = \begin{bmatrix} \varphi_{ds_1} \\ \varphi_{ds_2} \\ \varphi_{qs_1} \\ \varphi_{qs_2} \\ \varphi_{dr} \\ \varphi_{qr} \end{bmatrix} ; \quad [V] = \begin{bmatrix} V_{ds_1} \\ V_{ds_2} \\ V_{qs_1} \\ V_{qs_2} \end{bmatrix} \quad (28)$$

The equation of the electromagnetic torque is given

$$T_{em} = p \frac{L_m}{(L_m + L_r)} (\varphi_{dr} (i_{qs_1} + i_{qs_2}) + \varphi_{qr} (i_{ds_1} + i_{ds_2})) \quad (29)$$

The equations of flux are:

$$\Phi_{md} = L_s \left(\frac{\Phi_{ds_1}}{L_{s_1}} + \frac{\Phi_{ds_2}}{L_{s_2}} + \frac{\Phi_{dr}}{L_r} \right) \quad (30)$$

$$\Phi_{mq} = L_s \left(\frac{\Phi_{qs_1}}{L_{s_1}} + \frac{\Phi_{qs_2}}{L_{s_2}} + \frac{\Phi_{qr}}{L_r} \right) \quad (31)$$

Given that the “ dq ” axes are fixed in the synchronous rotating coordinates system, we have:

$$[A] = \begin{bmatrix} a_{11} & a_{12} & a_{13} & a_{14} & a_{15} & a_{16} \\ a_{21} & a_{22} & a_{23} & a_{24} & a_{25} & a_{26} \\ a_{31} & a_{32} & a_{33} & a_{34} & a_{35} & a_{36} \\ a_{41} & a_{42} & a_{43} & a_{44} & a_{45} & a_{46} \\ a_{51} & a_{52} & a_{53} & a_{54} & a_{55} & a_{56} \\ a_{61} & a_{62} & a_{63} & a_{64} & a_{65} & a_{66} \end{bmatrix} \quad (32)$$

$$[B] = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 1 \\ 0 & 0 & 0 & 1 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} \quad (33)$$

Where:

$$\begin{aligned}
 a_{11} &= a_{32} = \frac{R_{s1}L_a}{L_{s1}^2} - \frac{R_{s1}}{L_{s1}}; & a_{12} &= a_{34} = \frac{R_{s1}L_a}{L_{s1}L_{s2}}; & a_{56} &= -a_{65} = \omega_{gl} \\
 a_{11} &= a_{32} = -a_{31} = -a_{42} = \omega_s; & a_{14} &= a_{16} = a_{23} = a_{26} = a_{32} = a_{35} = 0; \\
 a_{41} &= a_{45} = a_{52} = a_{54} = a_{61} = a_{62} = 0; & a_{15} &= a_{36} = \frac{R_{s1}L_a}{L_{s1}L_r}; \\
 a_{21} &= a_{42} = \frac{R_{s2}L_a}{L_{s1}L_{s2}}; & a_{22} &= a_{44} = \frac{R_{s2}L_a}{L_{s2}^2} - \frac{R_{s1}}{L_{s1}} & a_{25} &= a_{46} = \frac{R_{s2}L_a}{L_rL_{s2}}; \\
 a_{51} &= a_{62} = \frac{R_rL_a}{L_{s1}L_r}; & a_{52} &= a_{64} = \frac{R_rL_a}{L_{s2}L_r} & a_{55} &= a_{66} = \frac{R_rL_a}{L_r^2} - \frac{R_r}{L_r};
 \end{aligned}$$

5 Simulations and Results Discussion

The simulation was carried out by keeping the supply voltage of the induction motor (i.e the output of the matrix converter) fixed and varying only the frequency f_o in order to be able to compare the motor performance for both strategies presented before. The six-phase matrix converter presented is being simulated for a desired output frequency of $f_o=50$ Hz, with a switching frequency of $f_s = 5$ KHz. Both converters are first feeding a passive R-L load ($R_s=20 \Omega$ and $L_r=0.04$ H) and then a 50 HP, 460 V double star induction motor driving a 100 N.m resistive torque.

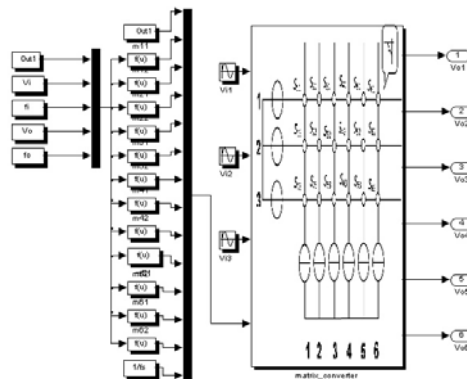


Figure 3

The matrix converter simulink®/Matlab diagram (Venturini method)

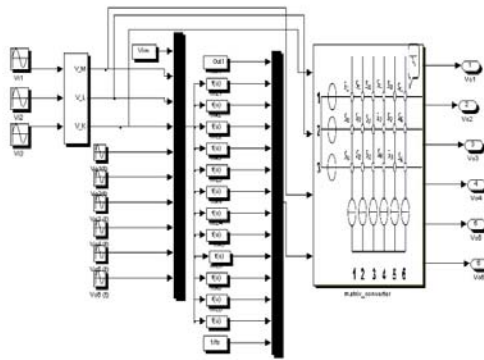


Figure 4

The matrix converter simulink®/Matlab diagram (Scalar strategy control)

5.1 Results Discussion

5.1.1 Results of the First Method ($f_o = 50$ Hz)

Figure 5 shows the matrix converter output voltage and its spectral analysis. The fundamental harmonic lies at the 50 Hz desired frequency and the higher order harmonics are in the neighbourhood of the 5 KHz switching frequency. The current form in a one phase of the R - L load (Figure 6), shows clearly that it approximates a sine wave shape at the desired frequency (50 Hz). It can be noted that the current shape in the case of a six-phase load illustrated in Figure 7 shows that the system is an unbalanced one.

Figure 8 represents a one phase stator current wave form. One can notice the presence of high oscillatory current, resulting from the large electromagnetic torque fluctuations as shows in Figure 10.

The variation of the rotor speed given in Figure 9, shows that its magnitude is not only slightly less than the rotating field speed, but also its shape is an oscillatory one.

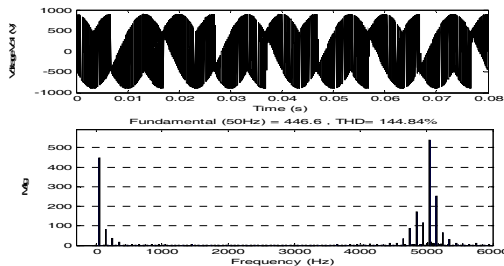


Figure 5

Voltage output and its FFT spectrum

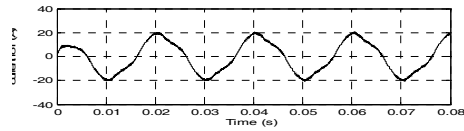


Figure 6

One phase R-L load current wave form

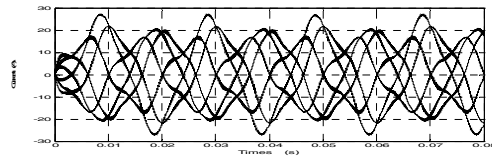


Figure 7

Six-phase R-L load current wave form

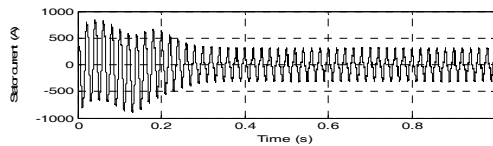


Figure 8

One phase stator current variation

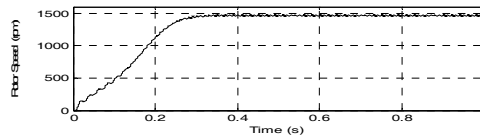


Figure 9

Rotor speed variation

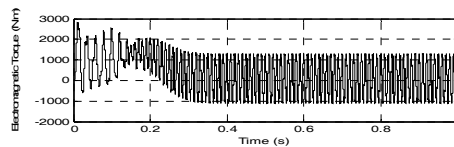


Figure 10

Electromagnetic torque variation

5.1.2 Results of the Second Method ($f_o = 50$ Hz)

Figure 11 represents the matrix converter voltage output and its spectral analysis. It shows a fundamental harmonic lying at the desired frequency (50 Hz) and higher order around the 5 KHz switching frequency.

Figure 12 represents the current form in a phase of the R - L load. This wave form is approaching the sine wave and is at the desired frequency of 50 Hz.

Figure 13 represents the current form in six-phase R-L load. It is visible that it represents a balanced six-phase system.

Figure 14 represents the one phase stator current wave form. In this case, the high oscillations have disappeared leading to a normal operating double star induction machine.

Figure 16 represents the electromagnetic torque wave form. This torque contains very reduced oscillations as that obtained from a balanced voltage system supplying the double star induction machine.

Figure 15 represents the rotor speed variation. This speed is slightly less than the rotating field speed.

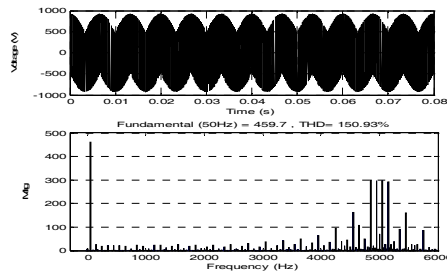


Figure 11

Voltage output and its FFT spectrum

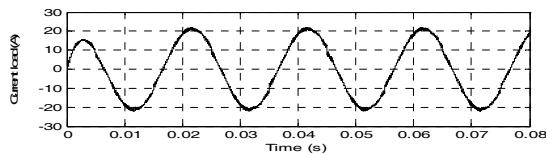


Figure 12

One phase R-L load current wave form

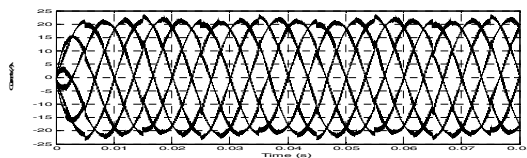


Figure 13

Six-phase R-L load current wave form

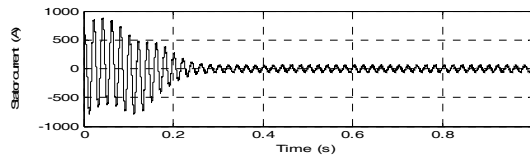


Figure 14

One phase stator current variation

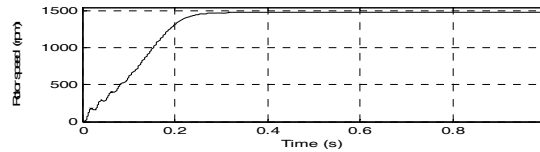


Figure 15

Rotor speed variation

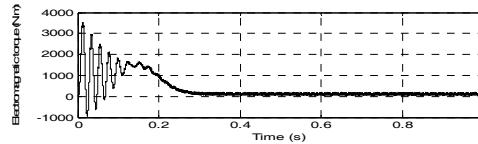


Figure 16

Electromagnetic torque variation

Conclusions

In the present paper, a comparative performance study between two different control strategies applied to a six-phase matrix converter is presented. The first strategy is derived from the Venturini method, and the second one is practically an extension of the scalar strategy control.

This comparative investigation is carried out using first an R-L load and then a double star induction machine. The obtained simulation results have been very useful and helpful in illustrating the merits of each method, though both strategies produce a six-phase voltage system with a load current at the 50 Hz desired frequency.

However, the Venturini method is simple and easy to implement. Unfortunately, the nature of the obtained voltage system is an unbalanced one and needs to be corrected and worked on to produce a balanced one. because an unbalanced voltage system has a direct impact on the motor's performance, giving important electromagnetic torque oscillations and high oscillatory currents in the steady state mode. On the other hand, the scalar strategy is more complex and produces, for the same magnitude, a balanced six-phase voltage system compared to the Venturini method.

References

- [1] Alesina A. and Venturini, M.; "Intrinsic Amplitude Limits and Optimum Design of 9-Switches Direct PWM AC-AC Converters" Power Electronics Specialists Conference, 1988. PESC '88 Record, 19th Annual IEEE, 11-14 Apr. 1988, pp. 1284 -1291 Vol. 2
- [2] G. Roy, G. E. April, "Cycloconverter Operation under a New Scalar Control Algorithm," in *Proc. IEEE PESC '89*, 1989, pp. 368-375
- [3] Bendiabdellah, A., Bachir, G.: "A Comparative Performance Study between a Matrix Converter and a Three-Level Inverter Fed Induction Motor", *Acta Electrotechnica Et Informatica*, No. 2, Vol. 6, 2006
- [4] Ghalem, Bachir; Azeddine Bendiabdallah; "A Comparative Study between Two Control Strategies for Matrix Converter" *Advances in Electrical and Computer Engineering Journal*, Vol. 9, No. 2, 2009, pp. 23-27
- [5] Bachir, G., Bendiabdellah, A.: "Scalar Control for a Matrix Converter" *Acta Electrotechnica Et Informatica*, No. 2, Vol. 9, 2009
- [6] Casadei, D.; Serra, G.; Tani, A.; Zarri, L.; "A Novel Modulation Strategy for Matrix Converters with Reduced Switching Frequency Based
- [7] D. Hadiouche, H. Razik, A. Rezzoug, "Stady and Star Simulation of Space Vector PWM Control of Double-Induction Motors", 2000 IEEE-CIEP, Acapulco, Mexico, pp. 42-47
- [8] J-P. Martin, E. Semail, S. Pierfederici, A. Bouscayrol, F. Meibody-Tabar et B. Davat." Space Vector Control of 5-Phase PMSM Supplied by 5 H-Bridge VSIs". Conference on Modeling and Simulation of Electric Machines, Converters and Systems (ElectrIMACS'02), Montreal (Canada), 2002
- [9] Singh, G. K, Pant, V, Singh, Y. P "Voltage Source Inverter Driven Multi-Phase Induction Machine" *Computers and Electrical Engineering* 29, pp. 813-834, 2003
- [10] Lipo, T. A, "A dq Model of a Six-Phase Induction Machine," *Int. conf. of Electrical Machines, ICEM, Athenes*, pp. 860-867, 1980
- [11] Incze, I. I. Szabo, Cs. Imecs, M. "Voltage-Hertz Strategy for Synchronous Motor with Controlled Exciting Field", *Intelligent Engineering Systems*, 2007, INES 2007, 11th International Conference on, pp. 247-252